

Corrosion-erosion behavior of new Fe-based coating materials for chlorine-rich biomass combustion: Role of Ni, Si and B

R. Pflumm¹, B. Adamczyk², M. C. Galetz¹
E-Mail: pflumm@dechema.de
Funded by AiF
Period: 1.4.2014-31.10.2016



Biomass to energy conversion: Characteristics

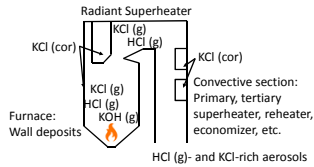


Fig. 1 Principal pathways of potassium and chlorine compounds in a biomass-fired boiler redrawn after [1]. (cor= corrosion, g= gas)

Corrosion

- ⇒ formation of porous, non-protective oxide scales
- Gaseous Cl and K compounds (via "active oxidation")
- Molten alkali chlorides (as dominant species) depositing
 - Sulfation of alkali chlorides or reaction between chlorides and metal
 - Formation of eutectics with low melting temperatures ⇒ fluxing of protective oxide scales

Erosion

⇒ removal of corrosion-resistant oxide layers followed by accelerated corrosion of the unprotected substrate [2-5]

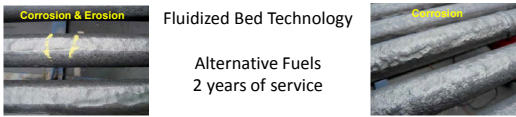


Fig. 2 Superheater tube damage due to corrosion and combined corrosion-erosion attack after corrosion layer removal (www.vivis.de under "Ersatzbrennstoff-Kraftwerke")

Improvement of the corrosion-erosion resistance via material design

- Empirical results ⇒ Ni-base alloys with ca. 20-23 wt.% Cr and 8-10 wt.% Mo (i.e. IN 625) ⇒ excellent corrosion resistance & low resistance against erosion
- New results regarding the material performance in Cl-rich environments at high temperatures [3-10]:
 - Carbides:** good against erosion & not corrosion resistant.
 - Chromia** scales form chromates in wet environments ($2KCl_s + 1/2Cr_2O_3 + H_2O_g + 3/4O_2_g \rightarrow K_2CrO_4 + 2HCl_g$)
 - Refractory metals and silicon** improve the corrosion and erosion resistance
 - Comparable amounts of **silicon** and **boron** (self-fluxing alloys) lead to coatings with reduced porosity
 - Iron** is not necessarily detrimental for the corrosion resistance

Approach: Model alloys ⇒ corrosion-erosion performance of the bulk materials

- Ingots obtained by centrifugal casting ⇒ coin-like samples via spark erosion
- Main issue: the influence Fe, Ni, Mo, and Si on the corrosion-erosion performance**
 - Nb, W and B were added in constant amounts
- IN 625 (Ni-21Cr-10Mo-3.5Nb-0.1Si...wt%) as reference

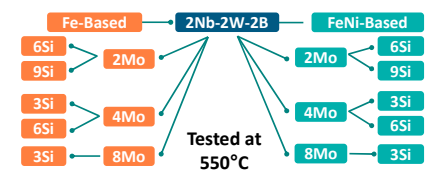


Fig. 3 Composition of the model alloys (wt.%)

Test 1: Corrosion Resistance (no Erosion)

7%O₂-17% H₂O-2,5% HCl rest N₂ → Simulated real biomass-firing atmosphere

- high Cl amount
- presence of water vapor

Test 2: Corrosion-erosion resistance

Lab air → 320°C → Sample → Cl-containing ash (ca. 200 g)

- Corrosion: Cl-, S-, K-, and Na-containing ash
- Erosion due to hard ash particles (SiO₂, Al₂O₃)

Results of test 1: Corrosion performance

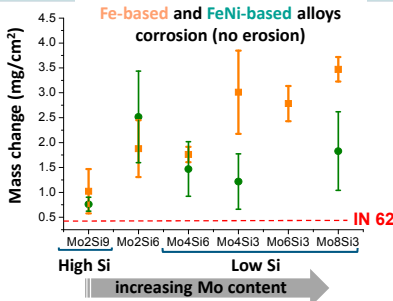


Fig. 5 (Test 1) Mass change after 1122 h at 550°C (common elements: Nb, W, and B; 30 wt% Ni)

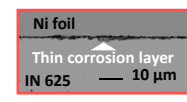


Fig. 6 Micrograph of the corrosion layer in the reference material (IN 625): Best performance for Cl corrosion in terms of mass gain

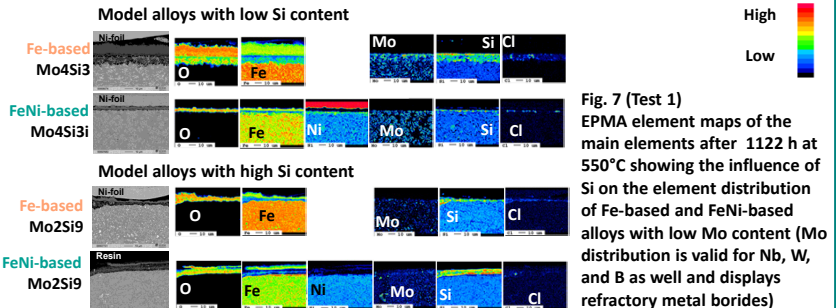


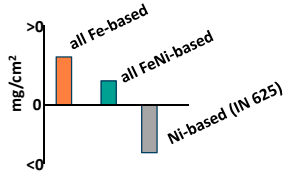
Fig. 7 (Test 1) EPMA element maps of the main elements after 1122 h at 550°C showing the influence of Si on the element distribution of Fe-based and FeNi-based alloys with low Mo content (Mo distribution is valid for Nb, W, and B as well and displays refractory metal borides)

Model alloys: Ni and Si have a significant influence on the thickness and morphology of the corrosion layers

Results Test 2: Corrosion-erosion performance

- No agglomeration of ash observed
- Spalled scale gets lost in the surrounding ash ⇒ therefore, qualitative mass change diagrams

Test 2: 332 h at 550°C



Test 2: 1052 h at 550°C

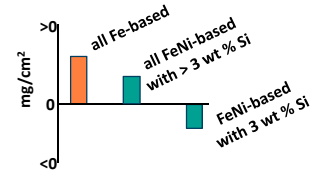


Fig. 8 (Test 2) Qualitative mass change diagrams of the model alloys. The mass change of IN 625 remains negative, therefore not shown in the left diagram.

- IN 625 develops a thin oxide layer ⇒ oxide removal followed by oxide growth phases ⇒ "oxidation-affected erosion" [3] ⇒ negative mass change
- Fe and FeNi alloys develop thicker oxide layers ⇒ partial damage, cracks, and local removal due to erosion ⇒ more diffusion paths, increased corrosion rate ⇒ "erosion-accelerated oxidation" [3] ⇒ positive mass change

Corrosion vs. corrosion-erosion performance

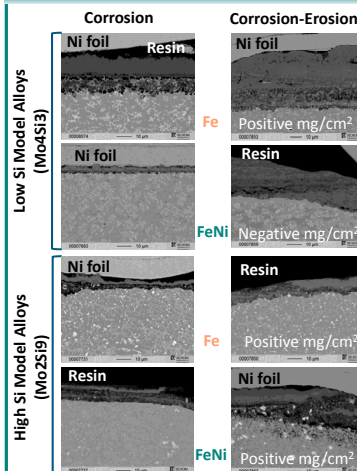


Fig. 9 Test 1 vs. Test 2: comparison between the corrosion scale morphologies

- Common elements: Nb, W, and B
- Refractory metal borides (i.e. white phases in grey scale micrographs) are resistant against Cl corrosion
- Duration of experiments > 1000 h
- Low Si model alloys:
 - Ni reduces the corrosion rate
 - Erosion enhances the corrosion rate of Ni-containing alloys
 - Fe-based (Ni-free) alloys ⇒ more resistant against corrosion-erosion
- High Si model alloys ⇒ comparable performance independent from the Ni content
- Decreasing the corrosion rate ⇒ no significant effect of Mo; Si is more effective
- Reference material IN 625:
 - Best performance for Cl corrosion
 - Worst performance for combined corrosion-erosion attack

[1] Nielsen [Progress in Energy and Combustion Science 26 2000] [2] Altobelli Antunes [Corrosion Science Nov 2013] [3] Kang C.T. et al. [Metall. Trans. A 18 1987] [4] Wang [Wear 188, 1995] [5] Norling [Wear 254 2003] [6] Galetz [Journal of Thermal Spraying and Technology Jan 2013] [7] Paul [Journal of Thermal Spraying and Technology Aug 2012] [8] Oksa [Journal of Thermal Spraying and Technology Mar 2013] [9] Israelsson [Oxid Met 83 2015] [10] Fujikawa [Mat Sci Eng A 120 1989]

Project partners: ¹DECHEMA-Forschungsinstitut, Theodor-Heuss-Allee 25, 60486 Frankfurt am Main

²Bundesanstalt für Materialforschung und -prüfung, Unter den Eichen 87, 12205 Berlin

Acknowledgements: Arbeitsgemeinschaft industrieller Forschungsvereinigungen "Otto von Guericke" e.V. is gratefully acknowledged for supporting this work.