

## Improvement of Oxidation Behavior of Ferritic-Martensitic Steels in Water Vapor **Containing Environments**







Modern heat resistant ferritic-martensitic steels are of great interest as superheater materials in fossil fuel power plants or as material for interconnectors in solid oxide fuel cells [1,2].

The environments of such applications contain high amounts of H<sub>2</sub>O, which is known to promote the formation of the volatile chromium species  $CrO_2(OH)_2$  leading to insufficient oxidation resistance of 9% Cr-steels in such atmospheres, due to quicker breakdown of the protective chromia layer, the so-called breakaway oxidation [3].

To apply ferritic-martensitic steels at temperatures above 600°C new corrosion protection systems must be developed.

Tab. 1: Composition of steels investigated

14

12

6

4

2

Fig. 4:

of

0+ 0

Am/A, [mg/cm 10 8

[wt%]	Gr	Mn	Ma	盛	e
P91	7.9 9.6	0.25 0.6	0.8 1.1	0	0.06 0.15
P92	8.5-9.5	0.5-0.6	85-0.8	1.6-2.0	0.07-0.15

- investigation of Cr<sub>2</sub>O<sub>3</sub>, Mn<sub>3</sub>O<sub>4</sub> and MnCr<sub>2</sub>O<sub>4</sub> in 1% O<sub>2</sub>, 10% H<sub>2</sub>O and N<sub>2</sub> at 650°C influence on the kinetics of oxidation
- reference samples from pure metal powder, which were pre-oxidized in synthetic air at 1000°C for 50h



- $Mn_3O_4$  was transferred to  $Mn_2O_3 \rightarrow$  great increase of mass during the initial phase of oxidation
- equilibrium is reached for longer exposure times mass becomes stable  $\rightarrow$ no evaporation determined in this environment
- corrosion test of  $\mathrm{Cr}_2\mathrm{O}_3$  in  $\mathrm{H}_2\mathrm{O}$  containing environment result in a mass decrease after time of 450 h
- mass loss can be explained by evaporation of the volatile chromium species CrO<sub>2</sub>(OH)<sub>2</sub>
- metallic Cr and Mn in a ratio of 1:1 oxidized to (MnCr<sub>2</sub>O<sub>4</sub>)-spinel phase during pre-oxidation
- spinel shows no significant change of weight in simulated combustion atmosphere at 650°C

## **DIFFUSION COATINGS**

**OXIDATION BEHAVIOR** 

1% O<sub>2</sub>, 10% H<sub>2</sub>O and N<sub>2</sub> at 650°C

significantly, no spallation in crucible

- Cr

Manganese Coated Sample

oxidation experiments in simulated combustion environment with

oxidation rate is initially very high, subsequently rate decreases

formation of rapidly growing surface manganese oxides,

however kinetics of further oxidation is very slow (see reference

0

9% Cr

oxides on top)  $\rightarrow$  evaporation of CrO<sub>2</sub>(OH)<sub>2</sub> inhibited

– Mn

10

- diffusion coating with manganese via pack cementation process
- substrate: P92, powder 5% Mn, 2% MnCl<sub>2</sub>, R Al<sub>2</sub>O<sub>3</sub>, T=1050°C, t=2 h, Ar/ Ha
- uniform diffusion layer with a thickness of around 15 µm
- line-scan of EPMA illustrates the concentration profiles of Mn, Cr and Fe
- Mn is diffused homogeneously into the metal subsurface regions
- no chromium could be detected in the outer coating layer, which is required to form the chromium-manganese-spinel phase



as-rec 5%Mn

10%Cr

800

600

400

time [h] weight change vs. time (1% O2,

10% H<sub>2</sub>O and N<sub>2</sub>, T=650°C)

formation of thin Cr2O3-scale on

underneath chromium enriched

zone even after 800 h of exposure

200

Chromium Coated Sample

chromium carbide

oxidation times

surprising kinetic stability

P91

1000

- diffusion coating with chromium via pack cementation process
- substrate: P92, powder 10% Cr, 5% MnCl<sub>2</sub>, R Al<sub>2</sub>O<sub>3</sub>, T=1050°C, t=2 h, Ar/ H<sub>2</sub>
- chromium carbide layer on surface (thickness: ~5um)
- chromium enriched zone underneath with a depth of around 75  $\mu m$
- no manganese was detected

wet above Cr<sub>23</sub>C

, way occurs below 7% Cr [3]

Fig. 6: model calculation of

acknowledged.

minimum Cr-concentration to

form Cr<sub>2</sub>O<sub>3</sub> scale at 650°C [3]

drv

in chromium enriched zone large ferrite grains had developed, that do not have a negative influence on the mechanical properties of the bulk material, because they are only present in the metal subsurface region



# **CONCLUSION AND OUTLOOK**

The improvement of oxidation behavior of ferriticmartensitic steels could be demonstrated.

The formation of a chromium-manganese-spinel surface on the substrate during high temperature exposure has not been successful yet due to the "low" temperature of 650°C.

The spinel formation starts at temperatures above 800°C. Therefore further samples will be coated with different powder compositions and afterwards a pre-oxidation at 1000°C will be executed.

For application of ferritic-martensitic steels e.g. in SOFCs deposition with other compositions and elements (e.g. Co) will be developed. These samples have to be investigated in oxidizing atmospheres above 800°C.

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### Fig. 6 illustrates the development position [µm] Cr-concentration for long Fig. 5: element concentration of oxidized chromium coated sample (P91)

100

<sup>80</sup> %

<u>ž</u> 60

40

0

atior

CODO 20 — Fe

- REFERENCES [1] Oehmingen, H.-G. et al. VDI- Bericht 1333. VDI- Verlag, Düsseldorf, 1997. Ennis, P.J. et al. VGB PowerTech 8. 2001, 87 [2]
- [3]

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