

Influence of interdiffusion zones on the performance of coatings against coking and metal dusting

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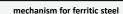


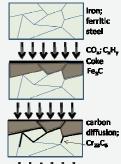
uncoated low alloy steel (1%Cr; 0.4%Mo) after 100 hrs under metal dusting conditions at 650°C (H₂-24%CO-2%H₂O)

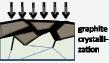
Metal Dusting Conditions

- temperatures between 400-900°C
- atmospheres with high carbon activity $a_c \ge 1$;
- low po2

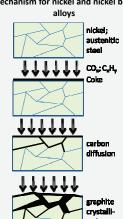
Metal Dusting Mechanisms





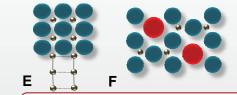


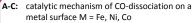
mechanism for nickel and nickel base



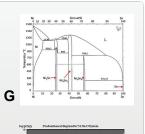
German Ministry of Economics via AiF unde IGF contract no. 16294N which is gratefully

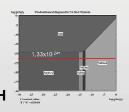
Functional Coating Approach



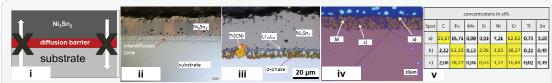


- D: poisoning of the catalyzed dissociation by the use of E:
- schematic of epitaxial graphite nucleation caused by matching the crystallographic parameters of graphite with Fe₃C and nickel insertion of large elements disturbs epitaxy
- the poisoning concept for high temperatures -Ni₃Sn₂-phase stable up to 1264°C
- oxidation stability of intermetallic Ni-Sn-phases





Coating Stability



The functional coating concept shown above relies on the constant chemical composition of the coating during operation time. Consequently, three different diffusion processes have to be controlled during operation time (i): no carbon is to diffuse through the coating to the substrate alloy; no substrate components should diffuse into the intermetallic coating; and no coating components, especially tin, should

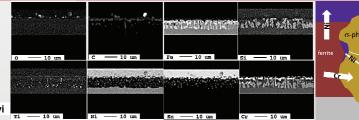
diffuse into the substrate. The Ni₃Sn₂-phase is inert to carburization, coking and metal dusting. Carbon is not able

to diffuse through the coating. Nickel and iron from the substrate can diffuse into the intermetallic coating in alloys with a chromium content lower than 15 wt%. This interdiffusion causes phase transformations from Ni₃Sn₂ to Ni₃Sn or $(Ni_{3-x}Fe_x)Sn_2$ with 0 < x < 1.5. These transformations lead to stresses and reduce the coating stability.

For substrates with a chromium content greater than 15 wt% the intermetallic nickeltin coating was found to be chemically stable for more than 3000hrs (ii). This can be associated with the high stability of the interdiffusion zone as is described in the following:

substrate

vii



The interdiffusion zone between the intermetallic coating and the substrate was intensively investigated for alloy 800, AISI 321 and alloy 600. For all three alloys, the interdiffusion zone was found to be a diffusion barrier consisting of chromium carbides, σ -phase as well as $\alpha\text{-ferrite}$ for the austenites (viii). Figures ii, iii, iv and vi show this zone in a cross-section of a nickel-tin coated alloy 800 specimen after 500 hrs exposure under metal dusting conditions at 620°C (H₂-24%CO-2%H₂O) produced using differential interference contrast (ii), electrochemically etched in 10M NaOH (iii), ZnSe-PVD coated (iv). Figure vi shows the element maps measured using EPMA. In table v EPMA-spot measurements of the positions highlighted as a)-c) in figure iv are listed; a) matches the $\text{Cr}_{23}\text{C}_6\text{-phase},$ b) $\sigma\text{-phase}$ and c) $\alpha\text{-}$ ferrite. The formation of these precipitates in the interdiffusion zone occurs due to the rapid depletion of nickel during the coating process in this zone. The nickel is consumed in the intermetallic nickel-tin coating leaving behind an iron-chromium rich layer (schematically shown in figure vii). This σ -phase rich layer was found to be a reliable diffusion barrier which stabilizes the chemical composition of the intermetallic coating for more than 3000hrs under metal dusting conditions

