

# Qualifying the Metastable, Biomedical $\beta$ -Titanium Alloy TiNb13Zr13 via Tuning of Gradiental Mechanical Properties and Partial Surface Modification

F. Depentori, W. Fürbeth  
e-mail: [depentori@dechema.de](mailto:depentori@dechema.de)  
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Background and problem	Approach
<ul style="list-style-type: none"> <li>• TiNb13Zr13 is a promising biomedical titanium alloy</li> <li>• the elastic modulus of 78 GPa is closer to that of bone (30 GPa) than Ti6Al4V</li> <li>• a femoral stem requires locally different mechanical and surface properties</li> </ul> <div style="display: flex; justify-content: space-around; align-items: center;"> <div style="border: 1px solid black; padding: 5px; background-color: #ffff00;"> <p>high strength wear resistance corrosion resistance</p> </div> <div style="border: 1px solid black; padding: 5px; background-color: #ffff00;"> <p>low elastic modulus biocompatibility corrosion resistance</p> </div> </div> <p>Fig. 1: requirements of a femoral stem for a hip implant<sup>1</sup></p>	<ul style="list-style-type: none"> <li>• tuning of different mechanical properties on upper and lower part of shaft → <math>\alpha</math>-precipitation, <math>\alpha'</math>-hardening or <math>\omega</math>-phase precipitation</li> <li>• different mode of anodizing, depending on needed surface properties</li> </ul> <div style="display: flex; justify-content: space-around; align-items: center;"> <div style="border: 1px solid black; padding: 5px; background-color: #ffff00;"> <p>Plasma Electrolytic Oxidation (PEO)</p> </div> <div style="border: 1px solid black; padding: 5px; background-color: #ffff00;"> <p>anodizing + hydroxyapatite (HA)</p> </div> </div> <p>Fig. 2: Schematic view of planned mechanical and chemical modification of TiNb13Zr13</p>

Mechanical and heat treatment	Corrosion testing	Anodizing, biocompatibility increase
<ul style="list-style-type: none"> <li>• cold forging of upper part of the stem → precipitation of <math>\alpha'</math>-phase (concept I)</li> <li>• hot forging and solution treatment of upper stem → precipitation of <math>\alpha</math>-phase (concept II)</li> <li>• hot forging and heat treatment in <math>\omega</math>-range → precipitation of <math>\omega</math>-phase (concept III)</li> </ul> <p>Fig. 3: TEM image of different phases in TiNb13Zr13 alloy<sup>2</sup></p>	<ul style="list-style-type: none"> <li>• electrochemical testing phase 1: base material concept I material concept II material concept III material → integral testing local testing</li> <li>• electrochemical testing phase 2: concept I, anodized concept II, anodized concept III, anodized → integral testing local testing</li> </ul> <p>→ Effect of different anodizing properties determined by local testing and investigation of boundary areas → AFM</p>	<ul style="list-style-type: none"> <li>• PEO for anodising upper stem part → anodizing voltages up to 400 V → dense and wear resistant oxide layer → different electrolytes</li> <li>• conventional anodizing of lower part of stem → simultaneous electrophoretic deposition of hydroxyapatite (HA) nanoparticles → increased biocompatibility due to incorporated, bone growth promoting material</li> </ul>

## Results

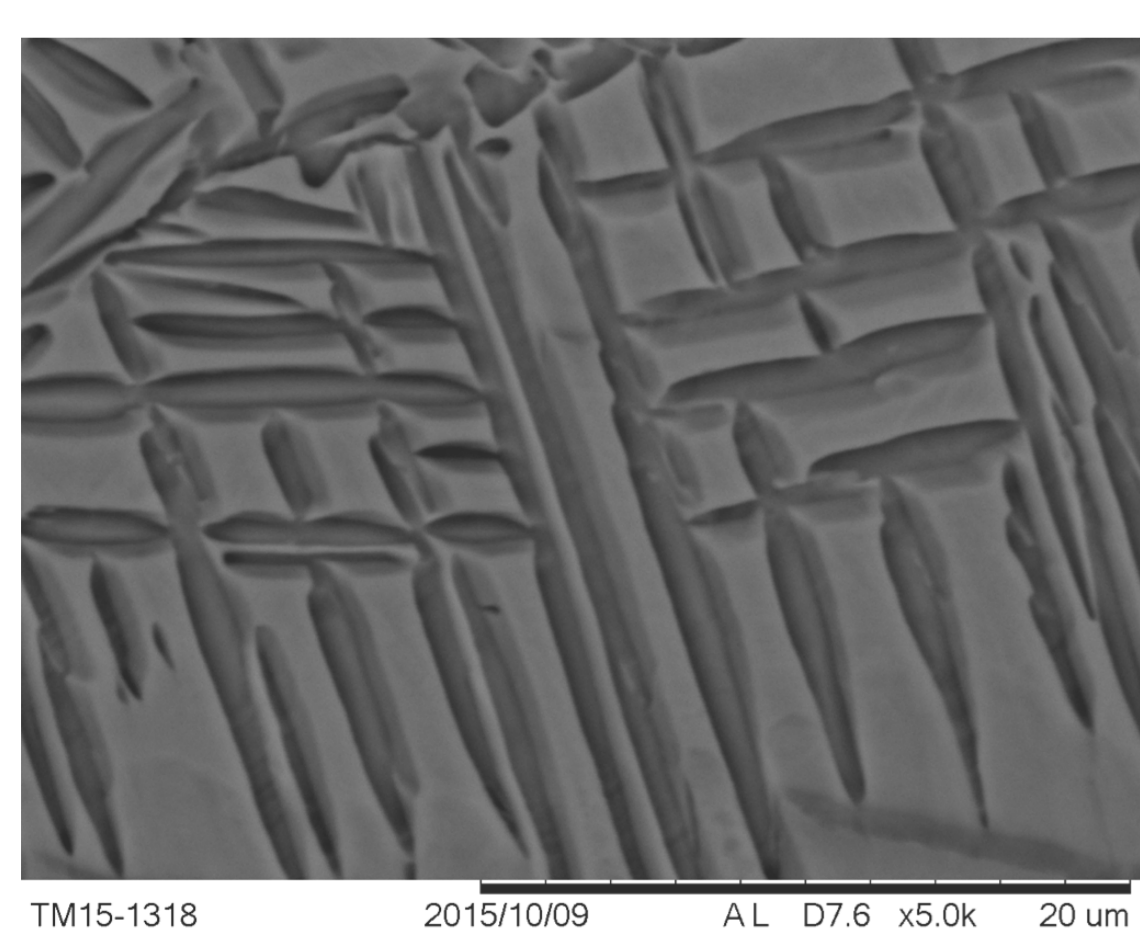


Fig. 4: SEM image of TiNb13Zr, 800 °C for 30 min, furnace cooled to 650 °C and held for 1 hour. Dark phase is assumed to be  $\alpha$ .

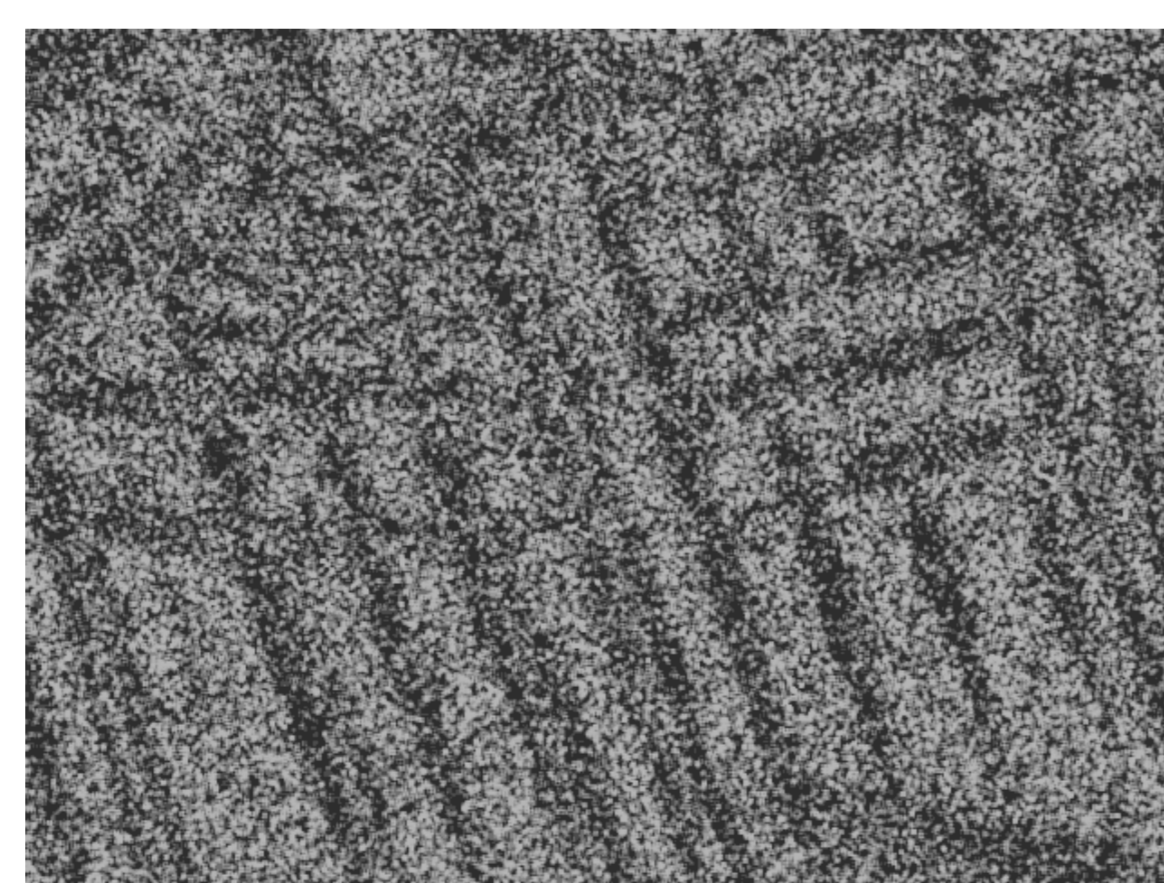


Fig. 5: Elemental mapping of Niobium from Fig. 4, showing diffusion of Nb out of the  $\alpha$ -phase.

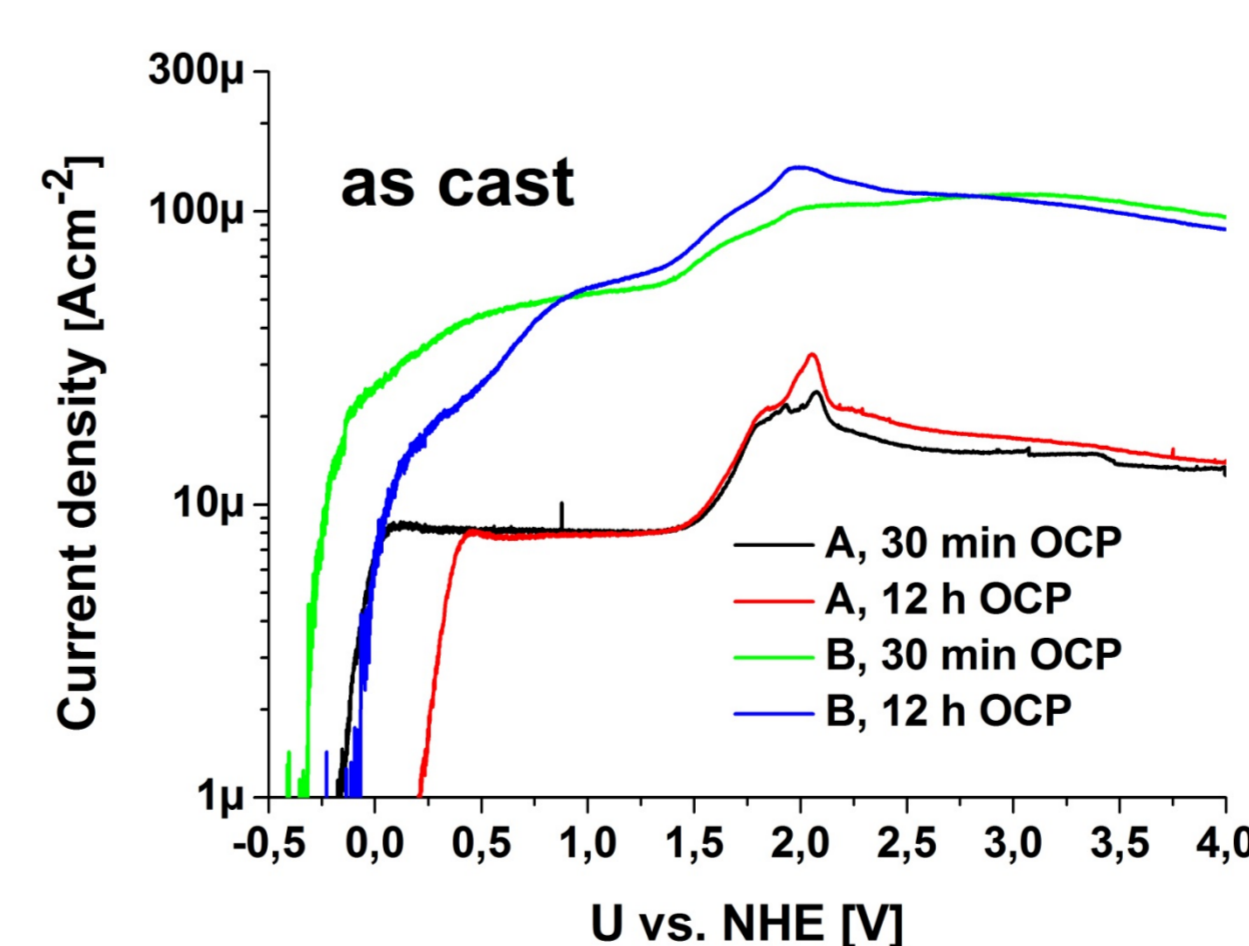


Fig. 6: Polarization curves of TiNb13Zr13, as cast. T = 37 °C, after 30 min and 12 hours. A: 1.5 wt% NaCl, B: 1.5 wt% NaCl + 1000 ppm F<sup>-</sup>.

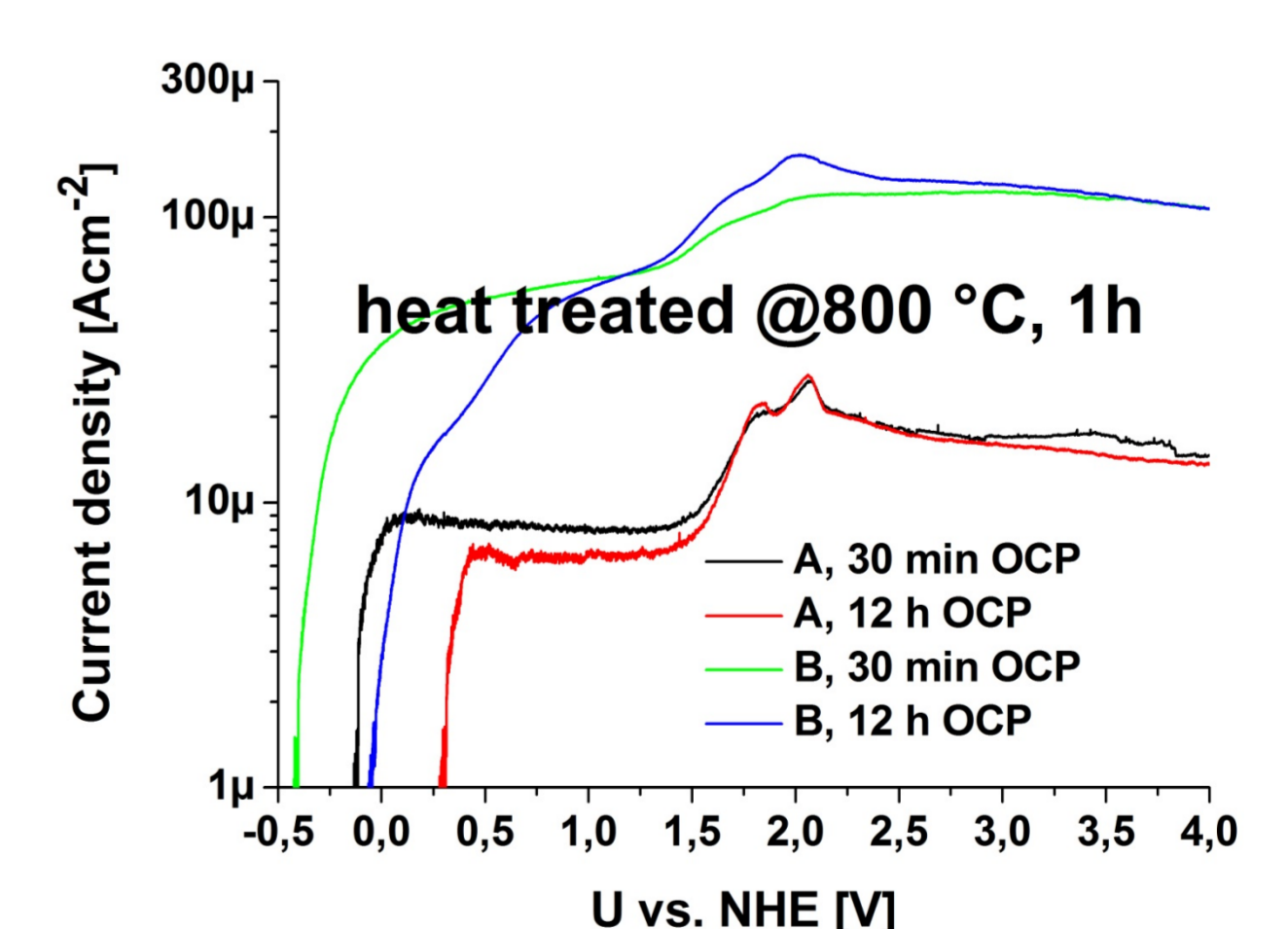
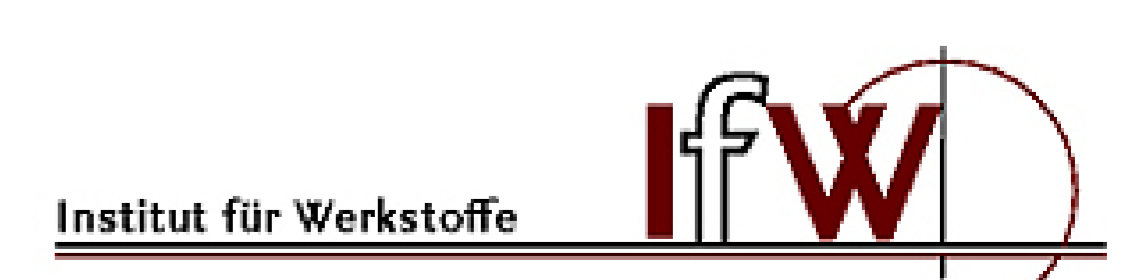


Fig. 7: Polarization curves of TiNb13Zr13, heat treated for one hour at 800 °C. A, B like in Fig. 6.

## Acknowledgements

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1) <http://www.bjj.boneandjoint.org.uk/content/93-B/5/665/F2.large.jpg>

2) S. Kobayashi et al., *Material Transactions*, Vol. 43, 12, 2002, 2962